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# Accelerated formation of barium titanate by solid-state reaction in water vapour atmosphere

Takahiro Kozawa, Ayumu Onda, Kazumichi Yanagisawa\*

Research Laboratory of Hydrothermal Chemistry, Faculty of Science, Kochi University, 2-5-1 Akebono-cho, Kochi 780-8520, Japan

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#### Abstract

Barium titanate (BaTiO<sub>3</sub>) powders were synthesized from commercially available raw materials (BaCO<sub>3</sub> and rutile) without particular mechanochemical processing by solid-state reactions in water vapour atmosphere. The formation rate of BaTiO<sub>3</sub> was accelerated by water vapour and single phase of BaTiO<sub>3</sub> was obtained by calcination at 700 °C for 4 h in water vapour atmosphere, though high temperature (850 °C for 2.5 h) was required by calcinations in air to complete the reaction. The formation kinetics followed the Valensi–Carter equation, which suggested that the reaction proceeded by a diffusion controlled process. The apparent activation energy for the formation of BaTiO<sub>3</sub> in air and water vapour atmosphere was estimated to be  $361 \pm 20$  kJ/mol and  $142 \pm 17$  kJ/mol, respectively. Water vapour is considered to enhance thermal decomposition of BaCO<sub>3</sub> and formation of BaTiO<sub>3</sub> by attacking surface Ti–O–Ti bonds in TiO<sub>2</sub>, increasing partial pressure of Ba(OH)<sub>2</sub>, and producing vacancies in the BaTiO<sub>3</sub> structure.

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## 1. Introduction

Barium titanate (BaTiO<sub>3</sub>) is well-known electroceramics widely utilized for manufactures of piezoelectric actuators and multilayer ceramic capacitors (MLCCs) due to its excellent dielectric properties. BaTiO<sub>3</sub> powders are conventionally prepared by solid-state reactions of barium carbonate (BaCO<sub>3</sub>) and titanium dioxide (TiO<sub>2</sub>) at temperatures above  $1000 \,^{\circ}$ C. The high calcination temperature required by the solid-state reaction process leads to many disadvantages of the BaTiO<sub>3</sub> powders, such as large particle size with a wide size distribution and high degree of particle agglomeration. Recent studies have clearly shown that the reduction of the particle size of the raw materials (BaCO<sub>3</sub> and TiO<sub>2</sub>) to submicrometer or even to nanoscale results in a significant decrease of the calcination temperatures.<sup>1–3</sup> By using the submicrometer BaCO<sub>3</sub> ( $d_{50} = 0.17 \,\mu\text{m}$ ) and fine TiO<sub>2</sub>  $(d_{50} = 0.2 \,\mu\text{m})$ , single phase of BaTiO<sub>3</sub> was almost obtained at 900 °C for 6 h.<sup>1</sup> The formation of BaTiO<sub>3</sub> by solid-state reactions of nanocrystalline BaCO<sub>3</sub> and TiO<sub>2</sub> powders was com-

0955-2219/\$ - see front matter © 2009 Elsevier Ltd. All rights reserved. doi:10.1016/j.jeurceramsoc.2009.05.031 pleted at 700–800 °C.<sup>2,3</sup> In addition, mechanochemical effects are known to be quite effective to reduce the calcination temperatures for solid-state reactions.<sup>4–7</sup> Kong et al.<sup>7</sup> milled the starting mixture in a planetary mill in air and obtained BaTiO<sub>3</sub> by calcination of the milled mixture at 800 °C for 2 h. The decrease of the calcination temperature provides the fine particle but usually lowers the crystallinity of the products.

On the other hand, it has been shown that the thermal decomposition of calcium carbonate (CaCO<sub>3</sub>) is accelerated by water vapour.<sup>8–11</sup> It is expected that the thermal decomposition of BaCO<sub>3</sub> is also promoted by water vapour and the subsequent formation of BaTiO<sub>3</sub> by solid-state reactions with TiO<sub>2</sub> is accelerated. The aim of this study is to prepare BaTiO<sub>3</sub> powders at low temperatures in water vapour atmosphere by solid-state reactions using commercially available raw materials without particular mechanochemical processing. In this paper, the influence of water vapour on the formation kinetics of BaTiO<sub>3</sub> is reported and its formation mechanism is discussed.

### 2. Experimental procedures

The commercially available BaCO<sub>3</sub> (Wako pure chemical industries, Japan, 99% purity,  $S_{\text{BET}} = 1.68 \text{ m}^2/\text{g}$ ,  $d_{\text{BET}} =$ 

<sup>\*</sup> Corresponding author. Tel.: +81 88 844 8352; fax: +81 88 844 8362. *E-mail address:* yanagi@kochi-u.ac.jp (K. Yanagisawa).

0.83 µm) and TiO<sub>2</sub> (rutile, Wako, 99% purity,  $S_{\text{BET}} = 5.60 \text{ m}^2/\text{g}$ ,  $d_{\text{BET}} = 0.25 \text{ µm}$ ) with stoichiometric quantities were mixed in a stainless ball mill for 6 h at 280 rpm. The mixed powder (0.1 g) was calcined at 650–1000 °C for 0.5–12 h in air and water vapour atmosphere by a tubular furnace equipped with a water evaporator. Calcinations in air atmosphere were performed in stagnant condition. In water vapour atmosphere, distilled water was introduced at a flow rate of 2 mL/min into the evaporator without a carrier gas to generate 100% water vapour atmosphere in the furnace. Flow rate of water vapour was estimated to be 2.5 L/min.

Crystalline phases in the products were identified by powder X-ray diffractions (XRD) obtained by a Rigaku Rotaflex RAD-RC diffractometer using Cu K $\alpha$  radiation operating at voltage and current of 40 kV and 100 mA, respectively. Data were collected in the range of 5–80° in  $2\theta/\theta$  scanning mode with a 0.02° step and scanning speed of 4°/min.

The amount of BaTiO<sub>3</sub> in each sample was determined from XRD peak areas of BaTiO<sub>3</sub> (101) (110) and silicon (111) diffraction. Silicon (Sigma–Aldrich, USA, 99.999% purity) was used as an internal standard. The calibration curve was previously obtained from the mixtures of silicon and pure BaTiO<sub>3</sub> which was prepared by solid-state reaction at 800 °C for 12 h, followed by calcination at 1200 °C for 6 h in air. TiO<sub>2</sub> was used as a dilution agent. Data were collected in the range of 27–33° in  $2\theta/\theta$  scanning mode with a 0.006° step and scanning speed of 0.5°/min.

The lattice constants were calculated by the least square method using silicon as an internal standard. Data were collected in the range of  $65-135^{\circ}$  in  $2\theta/\theta$  scanning mode with a  $0.006^{\circ}$  step and scanning speed of  $0.5^{\circ}/\text{min}$ . Specific surface area,  $S_{\text{BET}}$ , was measured by the BET method using nitrogen with a Yuasaionics NOVA-1200 instrument. The equivalent BET diameter,  $d_{\text{BET}}$ , was calculated by the following equation:

$$d_{\rm BET} = \frac{6}{\rho_{S_{\rm BET}}} \tag{1}$$

where  $\rho$  is the density of BaCO<sub>3</sub> 4.306 g/cm<sup>3</sup>, rutile type TiO<sub>2</sub> 4.250 g/cm<sup>3</sup> and BaTiO<sub>3</sub> 6.012 g/cm<sup>3</sup>.

### 3. Results and discussion

# 3.1. Preparation of BaTiO<sub>3</sub> powders by solid-state reactions

The formation of BaTiO<sub>3</sub> by solid-state reactions of BaCO<sub>3</sub> and TiO<sub>2</sub> involves the thermal decomposition of BaCO<sub>3</sub>, so that the forcible removing of CO<sub>2</sub> gas from the reaction field might be accelerated the formation of BaTiO<sub>3</sub>. The preliminary experiments for solid-state reactions of BaCO<sub>3</sub> and TiO<sub>2</sub> were conducted at 750 °C for 2 h in stagnant air and N<sub>2</sub> flowing atmosphere. N<sub>2</sub> gas was introduced to generate 100% N<sub>2</sub> gas flowing atmosphere in the furnace at the same flow rate of 2.5 L/min with that for 100% water vapour atmosphere. As shown in Fig. 1, the products obtained in stagnant air and N<sub>2</sub> flowing atmosphere gave the similar XRD patterns which showed that a large amount of BaCO<sub>3</sub> remained and a small amount of BaTiO<sub>3</sub> was

Fig. 1. XRD patters of the samples obtained by solid-state reaction at 750  $^{\circ}$ C for 2 h in (a) stagnant air and (b) N<sub>2</sub> atmosphere.

formed. We considered that a gas flow for forcible removing of  $CO_2$  gas had little effects on the decomposition of  $BaCO_3$ . Consequently, we examined the effect of water vapour atmosphere on the formation of  $BaTiO_3$  comparing with stagnant air atmosphere.

Fig. 2 shows the XRD patterns of the samples obtained by calcinations in air and water vapour atmosphere at 750 °C and 800 °C for 2 h. In air atmosphere, the raw materials remained in large quantities even at 800 °C. In contrast, the solid-state reaction of BaCO<sub>3</sub> and TiO<sub>2</sub> was accelerated by the injection of water vapour. BaTiO<sub>3</sub> was obtained as a single phase at 750 °C for 2 h in water vapour atmosphere. Water vapour accelerated the thermal decomposition of the BaCO<sub>3</sub> and then BaTiO<sub>3</sub> was synthesized at lower temperatures.

In order to investigate the reaction kinetics and formation mechanism of BaTiO<sub>3</sub>, quantitative analysis of BaTiO<sub>3</sub> in each sample was conducted by the XRD using the internal standard method. The formation ratios of BaTiO<sub>3</sub> (fraction reacted:  $\alpha$ ) are plotted against calcination time at various temperatures in Fig. 3. The single phase of BaTiO<sub>3</sub> was obtained in water vapour atmosphere by calcinations at 700 °C for 4 h and 750 °C for 2 h. However, the BaTiO<sub>3</sub> (1 0 1) (1 1 0) XRD peak area of these samples was slightly lower than that of fully crystallized BaTiO<sub>3</sub>, which results in lower formation ratios of these samples than 100%. The formation temperatures and times. The formation ratio by the calcinations in air has not reached 50% at 750 °C for 12 h, while that in water vapour atmosphere approached 100% at 700 °C within 12 h.

Tagawa and Igarashi<sup>12</sup> examined the kinetics of the solidstate reaction of strontium carbonate (SrCO<sub>3</sub>) and TiO<sub>2</sub> to form strontium titanate (SrTiO<sub>3</sub>) by the Jander<sup>13</sup> model and Valensi–Carter<sup>14,15</sup> model based on the diffusion controlled pro-





Fig. 2. XRD patterns of the samples obtained by solid-state reactions at  $750 \,^{\circ}$ C and  $800 \,^{\circ}$ C for 2 h in (a) air and (b) water vapour atmosphere.

cess. The reaction mechanism proposed by Jander is the simple model of powder reactions by diffusion but the equation proposed by Valensi and Carter was derived without simplification. We applied the Valensi–Carter equation to our experimental data and determined the mechanism for the solid-state reaction between BaCO<sub>3</sub> and TiO<sub>2</sub> to form BaTiO<sub>3</sub>.

The Valensi–Carter equation is given as following:

$$\frac{z - [1 + (z - 1)a]^{2/3} - (z - 1)(1 - a)^{2/3}}{z - 1} = kt$$
(2)

where z represents the volume of product formed per unit volume of reactant consumed,  $\alpha$  the fraction reacted, k the reaction rate constant, and t the reaction time. In the case of the reaction of BaCO<sub>3</sub> and TiO<sub>2</sub> to form BaTiO<sub>3</sub>, z is 0.600. Fig. 4 shows the Valensi–Carter plots for the reaction of BaCO<sub>3</sub> and TiO<sub>2</sub>. The linear relation was obtained for all data, which suggests that it is reasonable to conclude that the formation mechanism of BaTiO<sub>3</sub> in both atmospheres is diffusion controlled process following the Valensi–Carter equation. From the slopes in Fig. 4, the reaction



Fig. 3. Plots of fraction reacted of  $BaTiO_3$  ( $\alpha$ ) obtained in (a) air and (b) water vapour atmosphere versus calcination time at various temperatures. Solid symbols show that the product is the  $BaTiO_3$  single phase according to XRD.

rate constant, k, was obtained. Arrhenius plots of ln k versus 1/T as shown in Fig. 5 gave the apparent activation energy,  $E_a$ , for the formation of BaTiO<sub>3</sub> by the solid-state reactions and it was estimated to be  $361 \pm 20$  kJ/mol and  $142 \pm 17$  kJ/mol in air and water vapour atmosphere, respectively. By introducing water vapour, the apparent activation energy was drastically decreased. In other words, the diffusion of Ba<sup>2+</sup> and O<sup>2-</sup> ions through the BaTiO<sub>3</sub> layer was accelerated by water vapour.

### 3.2. Mechanism of accelerated reaction by water vapour

The results shown in Fig. 2 clearly indicated that water vapour accelerated the thermal decomposition of BaCO<sub>3</sub>. Wang and Thomson<sup>10</sup> described that adsorbed water vapour weakened Ca–CO<sub>3</sub> bond and the thermal decomposition of CaCO<sub>3</sub> was accelerated by water vapour. Water vapour atmosphere similarly might play an important role to weaken the Ba–CO<sub>3</sub> bond, which resulted in acceleration of BaCO<sub>3</sub> decomposition in water vapour atmosphere at lower temperatures in comparison with that in air. Furthermore, the lower CO<sub>2</sub> partial pressure



Fig. 4. Kinetics according to Valensi-Carter equation for reaction of BaCO<sub>3</sub> and TiO<sub>2</sub> in (a) air and (b) water vapour atmosphere.

in the water vapour might enhance the decomposition of BaCO<sub>3</sub> decomposition.

We previously showed that water adsorbed on the surface of amorphous titania particles catalyzed the rearrangement of the TiO<sub>6</sub> octahedra to accelerate the crystallization of amorphous titania to anatase.<sup>16,17</sup> MacKenzie<sup>18</sup> reported that water vapour assisted sintering of rutile type TiO<sub>2</sub> and presented an assumption of the formation of transient hydroxy-species such as Ti(OH)<sub>2</sub><sup>2+</sup> on the surface of the particles. The same effect is expected for the calcinations in water vapour atmosphere in this study. It is considered that water vapour attacks Ti–O–Ti bonds of rutile surface to promote rotation and movement of TiO<sub>6</sub> octahedra, and Ba<sup>2+</sup> and O<sup>2–</sup> ions which have already formed by the decomposition of BaCO<sub>3</sub>, easily react with TiO<sub>6</sub> octahedra to form BaTiO<sub>3</sub>. Most of formed hydroxyl groups are simultaneously eliminated as H<sub>2</sub>O molecule by the rearrangement of TiO<sub>6</sub> octahedra to the perovskite structure of BaTiO<sub>3</sub>.



Fig. 5. Arrhenius plot for BaTiO<sub>3</sub> formation.

The formation of BaTiO<sub>3</sub> must be limited to the BaCO<sub>3</sub>/TiO<sub>2</sub> contact points. The observed decrease of the reaction temperature in water vapour atmosphere even by using the relatively coarse particles (BaCO<sub>3</sub> 0.83  $\mu$ m and TiO<sub>2</sub> 0.25  $\mu$ m) may imply that a Ba species is efficiently supplied over the entire TiO<sub>2</sub> particle surface in water vapour atmosphere. One possible mechanism is gas phase transport. It is reported that the volatility of the barium oxide (BaO) is greatly increased by the presence of water vapour due to the formation of volatile hydroxide (Ba(OH)<sub>2</sub>) vapour<sup>19–21</sup> and Ba(OH)<sub>2</sub> vapour pressure is given as following<sup>21</sup>:

$$\ln K_{\rm p} = \frac{-16792.3}{T} + 4.94 \tag{3}$$

where  $K_p = p(Ba(OH)_2)/p(H_2O)$ . Though the Eq. (3) was obtained at high temperatures over 1000 °C, we can estimate Ba(OH)\_2 partial pressure to be  $2.2 \times 10^{-5}$  atm at 800 °C from the Eq. (3). This value is not negligible and gas phase transport of Ba(OH)\_2 could become important when the solid-state reaction occurs in water vapour atmosphere. Accordingly, the surface diffusion of barium may be enhanced in water vapour atmosphere.

The formation of BaTiO<sub>3</sub> by solid-state reactions is diffusion controlled process as described above, and is explained by coupled diffusion of  $Ba^{2+}$  and  $O^{2-}$  ions in the BaTiO<sub>3</sub> crystal lattice.<sup>3,22-24</sup> Mutin and Niepce<sup>23</sup> suggested vacancy mechanism for diffusion of  $Ba^{2+}$  and  $O^{2-}$  ions. It is reported that the BaTiO<sub>3</sub> powders prepared by hydrothermal method contain a large amount of proton in the oxygen sublattice and the proton defects are compensated by the simultaneously formation of barium and titanium vacancies.<sup>25</sup> These defects might be formed by the solid-state reactions in water vapour atmosphere, which can explain the enhanced solid-state diffusion of barium. Ba<sup>2+</sup> vacancies ( $(Ba_{1-x}H_{2x})TiO_3$ ) might be formed in the BaTiO<sub>3</sub> structure when Ba<sup>2+</sup> ions are diffused into the space between TiO<sub>6</sub> octahedra with hydroxyl groups, though most of formed hydroxyl groups are simultaneously eliminated as H<sub>2</sub>O molecule by the rearrangement of  $TiO_6$  octahedra to form BaTiO<sub>3</sub>. As a

Table 1 Specific surface area and corresponding particle size of BaTiO<sub>3</sub> powders.

Sample	Calcination	Atmosphere	$S_{\rm BET}~({\rm m^2/g})$	d <sub>BET</sub> (µm)
	conditions			0.00
1	800 °C/12 h	Aır	3.36	0.30
2	850 °C/3 h	Air	4.07	0.25
3	750 °C/2 h	Water vapour	4.14	0.24
4	750 °C/12 h	Water vapour	2.99	0.33
5	800 °C/2 h	Water vapour	4.04	0.25

result, the formation of  $Ba^{2+}$  vacancies facilitates the diffusion of  $Ba^{2+}$  ions by vacancy mechanism. On the other hand, it is also well known that sintering of  $BaTiO_3$  in reducing atmosphere forms  $O^{2-}$  ion vacancy ( $BaTiO_{3-x}$ ) with a valence reduction of titanium from  $Ti^{4+}$  into  $Ti^{3+}$ . In water vapour atmosphere that gives a reducing atmosphere compared with in air atmosphere,  $O^{2-}$  ion vacancy with the reduction of titanium ion might be formed in the  $BaTiO_3$  structure. This  $O^{2-}$  vacancy also promotes the diffusion of  $O^{2-}$  ions. Thus, it is considered that the diffusion of  $Ba^{2+}$  and  $O^{2-}$  ions to the  $TiO_2$  reaction front through the  $BaTiO_3$  layer is accelerated by vacancy mechanism with three different vacancies formed in water vapour atmosphere.

### 3.3. Powder properties and tetragonality

The specific surface area and particle size of selected BaTiO<sub>3</sub> powders prepared in this study are shown in Table 1. The results show that BaTiO<sub>3</sub> powders with the same or smaller particle size in comparison with those obtained in air were prepared in water vapour atmosphere by calcinations at lower temperatures for a shorter time. For example, the particle size of BaTiO<sub>3</sub> powder obtained by calcination at 750 °C for 2 h in water vapour atmosphere was estimated to be 0.24  $\mu$ m from its specific surface area, but 0.25  $\mu$ m by calcination at 850 °C for 3 h in air.



Fig. 6. Tetragonality of  $BaTiO_3$  as a function of calcination temperature for 12 h.

Fig. 6 shows the tetragonality (c/a) of BaTiO<sub>3</sub> obtained by calcinations at various temperatures for 12 h in air and water vapour atmosphere. BaTiO<sub>3</sub> was obtained as a single phase except for the sample obtained by calcination at 750 °C in air. In both atmospheres, the tetragonality of BaTiO<sub>3</sub> increased with an increase in the calcination temperatures, which is explained by the increase of BaTiO<sub>3</sub> crystallinity with increasing calcination temperatures. On the other hand, the tetragonality of BaTiO<sub>3</sub> single crystal (JCPDS No. 05-0626), by calcination at 850 °C. This result indicates that the crystallinity of BaTiO<sub>3</sub> is increased by water vapour.

### 4. Conclusions

BaTiO<sub>3</sub> powders were prepared by solid-state reactions of BaCO<sub>3</sub> and TiO<sub>2</sub> in air and water vapour atmosphere. The formation of BaTiO<sub>3</sub> was accelerated by water vapour and BaTiO<sub>3</sub> powders with the same or smaller particle size in comparison with those obtained in air were prepared in water vapour atmosphere by calcinations at lower temperatures for a shorter time. The solid-state reaction to form BaTiO<sub>3</sub> obeyed the Valensi-Carter equation, which suggested that the reaction proceeded by a diffusion controlled process. The apparent activation energy for the formation of BaTiO<sub>3</sub> in water vapour atmosphere was estimated to be  $142 \pm 17$  kJ/mol, much lower than that in air (361  $\pm$  20 kJ/mol). It is considered that water vapour has following effects to accelerate the formation of BaTiO<sub>3</sub>; (1) acceleration of BaCO<sub>3</sub> decomposition, (2) acceleration of BaTiO<sub>3</sub> formation by surface attacking of water at the  $TiO_2$ reaction front and by gas phase transport of Ba(OH)<sub>2</sub>, and (3) acceleration of the diffusion of Ba<sup>2+</sup> and O<sup>2-</sup> ions in the BaTiO<sub>3</sub> layer by formation of vacancies in the BaTiO<sub>3</sub> structure.

### References

- Hennings, D. F. K., Schreinemacher, B. S. and Schreinemacher, H., Solidstate preparation of BaTiO<sub>3</sub>-based dielectrics, using ultrafine raw materials. *J. Am. Ceram. Soc.*, 2001, 84, 2777–2782.
- Buscaglia, M. T., Bassoli, M., Buscaglia, V. and Alessio, R., Solid-state synthesis of ultrafine BaTiO<sub>3</sub> powders from nanocrystalline BaCO<sub>3</sub> and TiO<sub>2</sub>. J. Am. Ceram. Soc., 2005, 88, 2374–2379.
- Buscaglia, M. T., Bassoli, M., Buscaglia, V. and Vormberg, R., Solid-state synthesis of nanocrystalline BaTiO<sub>3</sub>: reaction kinetics and powder properties. J. Am. Ceram. Soc., 2008, 91, 2862–2869.
- Gomez-Yañez, C., Benitez, C. and Balmori-Ramirez, H., Mechanical activation of the synthesis reaction of BaTiO<sub>3</sub> from a mixture of BaCO<sub>3</sub> and TiO<sub>2</sub> powders. *Ceram. Int.*, 2000, 26, 271–277.
- Berbenni, V., Marini, A. and Bruni, G., Effect of mechanical milling on solid state formation of BaTiO<sub>3</sub> from BaCO<sub>3</sub>–TiO<sub>2</sub> (rutile) mixtures. *Thermochim. Acta*, 2001, **374**, 151–158.
- Yanagawa, R., Senna, M., Ando, C., Chazono, H. and Kishi, H., Preparation of 200 nm BaTiO<sub>3</sub> particles with their tetragonality 1.010 via a solid-state reaction proceeded by agglomeration-free mechanical activation. *J. Am. Ceram. Soc.*, 2007, **90**, 809–814.
- Kong, L. B., Ma, J., Huang, H., Zhang, R. F. and Que, W. X., Barium titanate derived from mechanochemically activated powder. *J. Alloys Comp.*, 2002, 337, 226–230.
- MacIntire, W. H. and Stansel, T. B., Steam catalysis in calcinations of dolomite and limestone fines. *Ind. Eng. Chem.*, 1953, 45, 1548–1555.

- Burnham, A. K., Stubblefield, C. T. and Campbell, J. H., Effects of gas environmental reactions in Colorado oil shale. *Fuel*, 1980, **59**, 871–877.
- Wang, Y. and Thomson, W. J., The effects of steam and carbon dioxide on calcite decomposition using dynamic X-ray diffraction. *Chem. Eng. Sci.*, 1995, **50**, 1373–1382.
- Agnew, J., Hampartsoumian, E., Jones, J. M. and Nimmo, W., The simultaneous calcination and sintering of calcium based sorbents under a combustion atmosphere. *Fuel*, 2000, **79**, 1515–1523.
- Tagawa, H. and Igarashi, K., Reaction of strontium carbonate with anatase and rutile. J. Am. Ceram. Soc., 1986, 69, 310–314.
- 13. Jander, W., Reaction in the solid state at high temperature I. Rate of reaction for an endothermic change. *Z. Anorg. Allg. Chem.*, 1927, **163**, 1–30.
- Carter, R. E., Kinetic model for solid-state reactions. J. Chem. Phys., 1961, 34, 2010.
- Frade, J. R. and Cable, M., Reexamination of the basic theoretical model for the kinetics of solid-state reaction. J. Am. Ceram. Soc., 1992, 75, 1949–1957.
- Yanagisawa, K., Yamamoto, Y., Feng, Q. and Yamasaki, N., Formation mechanism of fine anatase crystals from amorphous titania under hydrothermal conditions. J. Mater. Res., 1998, 13, 825–829.
- Yanagisawa, K. and Ovenstone, J., Crystallization of anatase from amorphous titania using the hydrothermal technique: effects of starting material and temperature. J. Phys. Chem. B, 1999, 103, 7781–7787.

- MacKenzie, K. J. D., The calcination of titania. VII. Sintering of rutile. *Trans. J. Br. Ceram. Soc.*, 1975, 74, 127–134.
- Stafford, F. E. and Berkowits, J., Mass-spectrometric study of the reaction of water vapor with solid barium oxide. J. Chem. Phys., 1964, 40, 2963–2969.
- Sasamoto, T., Mizushima, K. and Sata, T., Transpiration study of the reaction of water vapor with barium oxide. *Bull. Chem. Soc. Jpn.*, 1979, 52, 2127–2129.
- Ali (Basu), M., Mishra, R., Kerkar, A. S., Bharadwaj, S. R. and Das, D., Gibbs energy of formation of Ba(OH)<sub>2</sub> vapor species using the transpiration technique. *J. Nucl. Mater.*, 2001, **289**, 243–246.
- Beauger, A., Mutin, J. C. and Niepce, J. C., Synthesis reaction of metatitanate BaTiO<sub>3</sub>. Part 2: Study of solid–solid reaction interfaces. *J. Mater. Sci.*, 1983, 18, 3543–3550.
- Mutin, J. C. and Niepce, J. C., About stoichiometry of polycrystalline BaTiO<sub>3</sub> synthesized by solid–solid reaction. *J. Mater. Sci. Lett.*, 1984, 3, 591–592.
- Graff, A., Senz, S., Voltzke, D., Abicht, H.-P. and Hesse, D., Microstructure evolution during BaTiO<sub>3</sub> formation by solid-state reactions on rutile single crystal surfaces. *J. Eur. Ceram. Soc.*, 2005, 25, 2201–2206.
- Hennings, D. F. K., Metzmacher, C. and Schreinemacher, B. S., Defect chemistry and microstructure of hydrothermal barium titanate. *J. Am. Ceram. Soc.*, 2001, 84, 179–182.